

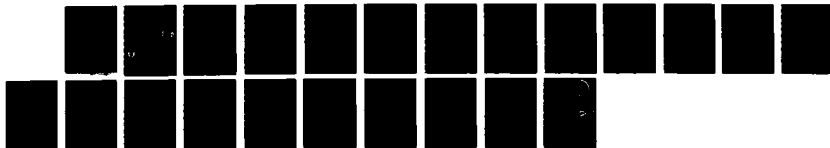
AD-A184 448

STOCHASTIC ANALYSIS FOR NAVIGATION OF AUTONOMOUS  
PLATFORMS USING RANGE FINDERS(U) ARMY ARMAMENT RESEARCH  
DEVELOPMENT AND ENGINEERING CENTER WTT C N SHEN  
AUG 87 ARCCB-TR-87020 F/G 17/5

1/1

UNCLASSIFIED

NL





AD-A184 448

DTIC FILE COPY

(12)

AD

TECHNICAL REPORT ARCCB-TR-87020

**STOCHASTIC ANALYSIS FOR NAVIGATION OF  
AUTONOMOUS PLATFORMS USING RANGE FINDERS**

C. N. SHEN

DTIC  
ELECTE  
SEP 10 1987  
S D

AUGUST 1987



**US ARMY ARMAMENT RESEARCH, DEVELOPMENT  
AND ENGINEERING CENTER  
CLOSE COMBAT ARMAMENTS CENTER  
BENÉT WEAPONS LABORATORY  
WATERVLIET, N.Y. 12189-4050**

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

87 9 9 290

#### DISCLAIMER

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

The use of trade name(s) and/or manufacturer(s) does not constitute an official indorsement or approval.

#### DESTRUCTION NOTICE

For classified documents, follow the procedures in DoD 5200.22-M, Industrial Security Manual, Section II-19 or DoD 5200.1-R, Information Security Program Regulation, Chapter IX.

For unclassified, limited documents, destroy by any method that will prevent disclosure of contents or reconstruction of the document.

For unclassified, unlimited documents, destroy when the report is no longer needed. Do not return it to the originator.

A184 448

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER ARCCB-TR-87020	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) STOCHASTIC ANALYSIS FOR NAVIGATION OF AUTONOMOUS PLATFORMS USING RANGE FINDERS		5. TYPE OF REPORT & PERIOD COVERED Final
7. AUTHOR(s) C. N. Shen		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS US Army ARDEC Benet Weapons Laboratory, SMCAR-CCB-TL Watervliet, NY 12189-4050		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS US Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 6111.01.91A0.0 PRON No. 1A6AZ601NMLC
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE August 1987
		13. NUMBER OF PAGES 14
		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)  Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES  Presented at the Workshop on Automation and Robotics for Military Applications, Huntsville, AL, 22-23 October 1986. Published in Proceedings of the Workshop.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)  Laser Range Finder Spline Functions Vision Systems Autonomous Vehicle		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  → For range finders having noncooperative targets and considerable measurement errors, a stochastic analysis is necessary to determine the differentials such as the gradient of a terrain during navigation of an autonomous platform. The angular measurement errors in elevation or azimuth contribute a deteriorated effect of the gradient estimate, especially when the terrain or target is far away. The smoothing of these gradients can be obtained by using an optimization method for approximation involving spline functions. This method (CONT'D ON REVERSE)		

20. ABSTRACT (CONT'D)

can be applied to solve the following problems: whether the platform can climb on the estimated in-path slope or whether it will tip over on the estimated cross-path.

UNCLASSIFIED

## TABLE OF CONTENTS

	<u>Page</u>
PROBLEM DESCRIPTION	1
OBJECTIVE FUNCTION FORMULATION	2
The Measure of Closeness	3
The Measure of Smoothness	4
STOCHASTIC EXPECTATION	5
Problem Formulation for Two-Dimensional Grid	6
Choice of An Approximating Function	8
Choice of the Smoothness Measure $z(\xi, \eta)$	9
Smoothing Integral	10
CONCLUSIONS	11

## LIST OF ILLUSTRATIONS

1. Top and side view of range finder.	12
2. Random noise in angle and range measurements.	13
3. Representation of function due to angular errors.	13



Accession For	
NTIS CRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution /	
Availability Codes	
Dist	Avail and/or Special
A-1	

## PROBLEM DESCRIPTION

The problem presented here is part of the investigations conducted for the design of the data acquisition and decision making system for an unmanned exploratory platform. As we know, it is necessary for the platform to be equipped with a data acquisition and a decision making system.

Usually, a laser range finder is chosen as a main sensing device which can determine the distance to a point within a certain accuracy. With reference to Figure 1, the terrain is scanned by varying the azimuth angle,  $\theta_j$ , and the elevation angle,  $\beta_i$ , of the laser beam in a discrete fashion. In general, the measurements are then available in the form of a "range matrix" as

$$M = \{m_{ij}\} \quad (1)$$

where  $i = 1, 2, \dots, N$ , correspond to the elevation angle,  $\beta_i$

$j = 1, 2, \dots, L$ , correspond to the azimuth angle,  $\theta_j$

The range matrix  $M$  above describes a certain scanned area of the ground in front of the mobile robot platform and can be used to detect edges of discrete objects or to estimate the slopes of the terrain. This is a two-dimensional grid. In our study for simplicity, a one-dimensional case is first considered, that is, change  $\beta_i$  for a fixed  $\theta_j$ . Thus, we have observation data  $m_i$  corresponding to  $\beta_i$ , from which we can estimate the in-path slopes of the range.

Generally speaking, both  $\beta_i$  and  $m_i$  are subject to random errors such that

$$\beta_i = \xi_i + v_i \quad (2)$$

$$m_i(\beta_i) = f(\beta_i) + \mu_i \quad (3)$$

where

$$\xi_i \text{ are known knots;} \quad (4a)$$

$$f(\xi) \text{ is an unknown function;} \quad (4b)$$

$$\beta_i \text{ are stochastic intervals;} \quad (5a)$$

$$m_i(\beta_i) \text{ are measurements corrupted by noise;} \quad (5b)$$



$v_i$  and  $\mu_i$  are random errors with zero means, for all  $i = 1, 2, \dots, N$ .

Equations (2) and (3) imply that both independent and dependent variables are corrupted by random noise, which may make the problem more complicated, as shown in Figure 2.

With the nodal described above, we are now able to formulate the problem.

#### OBJECTIVE FUNCTION FORMULATION

Referring to Figure 3, it is apparent that we cannot use the method of interpolation directly to approximate the unknown function  $f$  since the  $\beta_i$  are stochastic. Instead of this, we would like to estimate  $f$  by an approximating function  $h$ ; our objective is to determine the values of function  $h$  and its first derivatives due to random angle error  $v_i$ .

The following relations can be derived by using Taylor's series expansion at  $\beta_i$ :

$$f(\beta_i) = f(\xi_i) + \frac{df(\xi_i)}{d\xi} v_i + o(v_i) \quad (6)$$

where  $o(v)$  represents the higher order term of  $v$ . Using the first-order approximation yields:

$$f(\beta_i) \approx f(\xi_i) + \frac{df(\xi_i)}{d\xi} v_i \quad (7)$$

Similarly, for the approximating function  $h$  to estimate the unknown function  $f$ , we have

$$h(\beta_i) \approx h(\xi_i) + \frac{dh(\xi_i)}{d\xi} v_i \quad (8)$$

From the equations above, one obtains

$$\lambda_i = h(\beta_i) - h(\xi_i) = \frac{dh(\xi_i)}{d\xi} (v_i) \quad (9)$$

The stochastic difference  $\lambda_i$  for the approximating function  $h$  should be as small as possible in this problem.

We will attempt to determine a function approximation  $h$  with a compromise between the following objectives:

1. The measurement value  $m_i$  should be fitted close enough.
2. The approximating function  $h$  should be smooth enough in the sense that the discontinuities in its second derivative are as small as possible.

Now in order to be able to formulate this criterion mathematically, we need to find some measure of smoothness and some measure of closeness of fit. To be more specific, suppose that  $L$  is a linear space of "smooth" functions and that  $J_C$  is a functional defined on  $L$  which measures how well a function fits the data. Suppose in addition that  $J_S$  is a functional defined on  $L$  which measures the smoothness of an element on  $L$ , then the smoothing problem is the following: find  $s \in L$ , such that

$$J(s) = \inf_{h \in L} J(h) \text{ or } J(s) \leq J(h) \quad (10)$$

where

$$J(h) = J_C(h) + J_S(h) \quad (11)$$

### The Measure of Closeness

From Figure 3, in order to fit data  $(v_i, m_i)$  as closely as possible, we can simply take the sum of squared errors from Eqs. (3) and (9) as a measure of closeness of fit  $J_C$ , that is

$$J_C = \sum_{i=1}^N \left( v_i \frac{dh}{d\xi} \right)^T \hat{R}_i^{-1} \left( v_i \frac{dh}{d\xi} \right) + \sum_{i=1}^N [h(\xi_i) - m_i(\xi_i)]^T \hat{R}_i^{-1} [h(\xi_i) - m_i(\xi_i)] \quad (12)$$

where from Eq. (3)

$$R_i \triangleq E[\mu_i \mu_i^T] \quad (13)$$

Here,  $R_i^{-1}$  and  $\hat{R}_i^{-1}$  are weighing matrices which reflect our degree of confidence in the data  $m_i$  and  $v_i$ . For convenience, it is assumed that  $R_i$  and  $\hat{R}_i$  are constants for all  $i = 1, 2, \dots, N$ .

From Eq. (9), the error  $\lambda_i$  due to the random noise  $v_i$  can be written as

$$\lambda_i = \frac{dh(\xi_i)}{d\xi} v_i \quad (14)$$

It is assumed that the random noise  $v_i$  is a certain stochastic process with zero mean as studied in the next section. Thus, the error covariance matrix for  $\lambda_i$  is

$$E[\lambda_i \lambda_i^T] = \frac{dh(\xi_i)}{d\xi} E[v_i v_i^T] \left[ \frac{dh(\xi_i)}{d\xi} \right]^T \quad (15)$$

### The Measure of Smoothness

From the viewpoint of the approximation theory, the spline function provides a means of optimally reconstructing an unknown function  $f$  such that

$$\int_{\xi_1}^{\xi_N} [s^2(\xi)]^2 d\xi \leq \int_{\xi_1}^{\xi_N} [h^2(\xi)]^2 d\xi = J_s \quad (16)$$

where  $s$  is a spline function,  $s \in C^2$ , and  $h$  is an approximation function of the unknown function  $f$  and  $h \in C^2$ . Thus,  $s(\xi)$  is the function, among those satisfying some constraints, that is "smoothest" in the sense of Eq. (16).

To be more convenient and simpler, in our study we will use the piecewise cubic spline  $s \in C^2$ . Then Eq. (16) can be rewritten as

$$J_s = \rho \sum_{i=1}^N \int_{\xi_{i-1}}^{\xi_i} [h(\xi)]^2 d\xi \quad (17)$$

In summary, substituting Eqs. (12) and (17) into Eq. (11) yields an objective functional J

$$J = \sum_{i=1}^N [h(\xi_i) - m_i]^T R_i^{-1} [h(\xi_i) - m_i] + \sum_{i=1}^N \left( \frac{dh}{d\xi} v_i \right)^T \hat{R}_i^{-1} \left( \frac{dh}{d\xi} v_i \right) + \rho \sum_{i=1}^N \int_{\xi_{i-1}}^{\xi_i} [h(\xi)]^2 d\xi \quad (18)$$

where  $\rho > 0$  is a smoothing parameter.

### STOCHASTIC EXPECTATION

Since  $v_i$  is a stochastic variable, we use the expected value of J,  $E[J]$ , as the functional to be minimized, i.e.,

$$E[J] = E \left\{ \sum_{i=1}^N [h(\xi_i) - m_i]^T R_i^{-1} [h(\xi_i) - m_i] + \sum_{i=1}^N \left( \frac{dh}{d\xi} v_i \right)^T \hat{R}_i^{-1} \left( \frac{dh}{d\xi} v_i \right) + \rho \sum_{i=2}^N \int_{\xi_{i-1}}^{\xi_i} [h(\xi)]^2 d\xi \right\} \quad (19)$$

where h is a set of any piecewise cubic Hermite polynomials and  $h \in C^1$ .

In order to obtain the solution to Eq. (19), the following algebraic manipulations for Eq. (19) are necessary:

$$\text{Define } h_i = h(\xi_i) \quad , \quad \dot{h}_i = \dot{h}(\xi_i)$$

$$E[J] = \sum_{i=1}^N [(h_i - m_i)^T R_i^{-1} (h_i - m_i) + E(v_i^T \dot{h}_i \hat{R}_i^{-1} \dot{h}_i v_i)] + \rho \sum_{i=2}^N \int [h(\xi)]^2 d\xi \quad (20)$$

Using the matrix identity, the second term of the above equation becomes

$$E(v_i^T \dot{h}_i \hat{R}_i^{-1} \dot{h}_i v_i) = \text{Trace} [(\dot{h}_i \hat{R}_i^{-1} \dot{h}_i) E(v_i v_i^T)]$$

and

$$E(v_i v_i^T) = \Delta \sigma^2 \quad (21)$$

Then,

$$E[J] = \sum_{i=1}^N (h_i - m_i)^T R_i^{-1} (h_i - m_i) + \text{Trace}[(\dot{h}_i^T \hat{R}_i^{-1} \dot{h}_i) E(v_i v_i^T)]$$

$$= \sum_{i=1}^N [(h_i - m_i)^T R_i^{-1} (h_i - m_i) + (\sigma_i \dot{h}_i)^T \hat{R}_i^{-1} (\sigma_i \dot{h}_i)] + \rho \sum_{i=2}^N \int_{\xi_{i-1}}^{\xi_i} [h(\xi)]^2 d\xi \quad (22)$$

As mentioned previously, our main purpose is to obtain the estimates of the values of the unknown function and its first derivatives at grids  $\xi_i$ ,  $i=1,2,\dots,N$ , i.e.,  $h(\xi_i)$  and  $\dot{h}(\xi_i)$ . To make the problem simpler, it is proposed that the state variable approach be used. Thus the optimization problem in Eq. (19) can be transformed into a state estimation problem, where each state vector  $x_i$  is defined as:

$$x_i = [h(\xi), \dot{h}(\xi)]^T \big|_{\xi_i} \quad (23)$$

Hence, the objective functional  $J$  becomes

$$E[J] = \sum_{i=1}^N [(\bar{H}x_i - m_i)^T \bar{R}_i^{-1} (\bar{H}x_i - m_i) + (\tilde{H}x_i)^T \hat{R}_i^{-1} (\tilde{H}x_i)]$$

$$+ \rho \sum_{i=2}^N \int_{\beta_{i-1}}^{\beta_i} [p(\xi)]^2 d\xi \quad (24)$$

where

$$\bar{H} = [1, 0], \quad \tilde{H} = [0, \sigma_i] \quad (25)$$

Now the key to solving the problem in Eq. (24) is to evaluate the smoothing integral so as to obtain an expression in terms of state variables.

#### Problem Formulation for Two-Dimensional Grid

When the observation data are noise corrupted and the underlying system is unknown, it is proposed to approximate the original signal by spline functions which minimize a certain objective function. Thus, from a set of discrete measurements,  $m_{i,j}$ , corrupted by the white noise process,  $v_{i,j}$

$$m_{i,j}(\beta_i, \theta_j) = f(\beta_i, \theta_j) + u_{i,j}, \quad i = 1, 2, \dots, N \quad j = 1, 2, \dots, N \quad (26)$$

with angle errors

$$\beta_i = \xi_i + v_i \quad \text{and} \quad \theta_j = \eta_j + u_j \quad (27)$$

The original two-dimensional signal  $f(\xi, \eta)$  defined in the region of  $(\xi, \eta)$  is approximated by a spline function  $s(\xi, \eta)$  which minimizes the following objective function:

$$J = J_C + J_S \quad (28)$$

where

$$\begin{aligned} J_C = & \sum_{j=1}^M \sum_{i=1}^N [s(\beta_i, \theta_j) - m_{i,j}]^T R_{i,j}^{-1} [s(\beta_i, \theta_j) - m_{i,j}] \\ & + \sum_{j=1}^M \sum_{i=1}^N [s(\beta_i, \theta_j) - s(\xi_i, \eta_j)]^T \hat{R}_{ij}^{-1} [s(\beta_i, \theta_j) - s(\xi_i, \eta_j)] \end{aligned} \quad (29)$$

and

$$J_S = \rho \left[ \int_{\eta_1}^{\eta_M} \int_{\xi_1}^{\xi_N} z(\xi, \eta) d\xi d\eta \right] \quad (30)$$

where  $\rho > 0$  is the smoothing parameter;  $R_{i,j} = E[\mu_{ij} \mu_{ij}^T]$  is the observation error covariance; and  $z(\xi, \eta)$  is a certain smoothness measure of  $s(\xi, \eta)$  at  $(\xi, \eta)$ .

The following relation can be derived by using Taylor's series expansion at  $(\beta_i, \theta_j)$ :

$$s(\beta_i, \theta_j) - s(\xi_i, \eta_j) = \frac{\partial s}{\partial \xi}(\xi_i, \eta_j) v_i + \frac{\partial s}{\partial \eta}(\xi_i, \eta_j) u_j + o(v_i) o(u_j) \quad (31)$$

Since  $v_i$  and  $u_j$  are stochastic variables, we will use the expected value of  $J_C$ ,  $E(J_C)$  as the functional to be minimized.

Define

$$s_\xi(i, j) = \frac{\partial s}{\partial \xi}(\xi_i, \eta_j) \quad (32)$$

$$s_\eta(i, j) = \frac{\partial s}{\partial \eta}(\xi_i, \eta_j) \quad (33)$$

We have

$$\begin{aligned}
 E[J_C] = & \sum_{j=1}^M \sum_{i=1}^N \{ [s(i,j) - m_{ij}]^T R_{ij}^{-1} [s(i,j) - m_{ij}] \\
 & + [\sigma_i s_\xi(i,j)]^T \tilde{R}_{ij}^{-1} [\sigma_i s_\xi(i,j)] \\
 & + [\Omega_j s_\eta(i,j)]^T \hat{R}_{ij}^{-1} [\Omega_j s_\eta(i,j)] \}
 \end{aligned} \quad (34)$$

where

$$\sigma_i^2 = E[v_i v_i^T] \quad (35)$$

and

$$\Omega_j^2 = E[u_j u_j^T] \quad (36)$$

#### Choice of An Approximating Function

In this report, we are interested in obtaining smoothed estimates of function values and the first derivatives in both  $\xi$  and  $\eta$  directions. Here, we propose to restrict our approximating functions to piecewise bicubic Hermite polynomials which have continuous first derivatives in both  $\xi$  and  $\eta$  directions.

Let us define

$$x_{i,j}^\Delta = [s(\xi, \eta), \frac{\partial s}{\partial \xi}(\xi, \eta), \frac{\partial s}{\partial \eta}(\xi, \eta), \frac{\partial^2 s}{\partial \xi \partial \eta}(\xi, \eta)]^T_{(\xi_i, \eta_j)} \quad (37)$$

for  $i = 1, 2, \dots, N$  and  $j = 1, 2, \dots, M$ . Then a piecewise bicubic Hermite polynomial is completely defined by  $x_{i,j}$ ,  $i = 1, 2, \dots, M$  as follows:

$$s(\xi, \eta) = s_{i,j}(\xi, \eta), \quad \text{for } \xi_i \leq \xi \leq \xi_{i+1} \quad (38)$$

and

$$\eta_j \leq \eta \leq \eta_{j+1} \quad (39)$$

Thus,  $s_{i,j}(\xi, \eta)$  can be written in terms of the basis functions  $\phi$  and  $\psi$ , which are the bicubic Hermite polynomials (spline functions), as follows:

$$s_{i,j}(\xi, \eta) = \sum_{l=0}^1 \sum_{m=0}^1 \begin{bmatrix} \phi_l(\xi) \cdot \phi_m(\eta) \\ \psi_l(\xi) \cdot \phi_m(\eta) \\ \phi_l(\xi) \cdot \psi_m(\eta) \\ \psi_l(\xi) \cdot \psi_m(\eta) \end{bmatrix}^T \cdot x_{i+l, j+m} \quad (40)$$

Then Eq. (34) becomes

$$\begin{aligned} E[J_C] = & \sum_{j=1}^M \sum_{i=1}^N \{ [Hx_{i,j} - m_{i,j}]^T R_{ij}^{-1} [Hx_{i,j} - m_{i,j}] \\ & + [\tilde{H}_i x_{ij}]^T \tilde{R}_{ij}^{-1} [\tilde{H}_i x_{ij}] \\ & + [\hat{H}_j x_{ij}]^T \hat{R}_{ij}^{-1} [\hat{H}_j x_{ij}] \} \end{aligned} \quad (41)$$

where

$$H = [1 \ 0 \ 0 \ 0] \quad (42)$$

$$\tilde{H}_i = [0 \ \sigma_i \ 0 \ 0] \quad (43)$$

$$\hat{H}_j = [0 \ 0 \ \Omega_j \ 0] \quad (44)$$

#### Choice of the Smoothness Measure $z(\xi, \eta)$

Here we present three examples of the smoothness measures and compare their physical implications.

1. Gaussian curvature: The mean curvature of a surface at  $(\xi, \eta)$  is defined as:

$$(0.5) \nabla^2 s(\xi, \eta) \quad (45)$$

Noting in Euler's theorem that the sum of two curvatures in perpendicular directions at a point is constant, the square of  $\nabla^2 s(\xi, \eta)$  in Eq. (45) would be a reasonable measure for the smoothness of a surface

$$z(\xi, \eta) = \left[ \frac{\partial^2}{\partial \xi^2} s(\xi, \eta) + \frac{\partial^2}{\partial \eta^2} s(\xi, \eta) \right]^2 \quad (46)$$



2. A variation from the Gaussian curvature: With reference to Eq. (46), an interesting case occurs when the two principal curvatures are equal and of the opposite sign. The mean curvature in this case is zero. This is the so-called "saddle point" and every surface element of such a membrane is "pure twist." An appropriate smoothness measure would be changed to:

$$z(\xi, \eta) = \left[ \frac{\partial^2}{\partial \xi^2} s(\xi, \eta) \right]^2 + \left[ \frac{\partial^2}{\partial \eta^2} s(\xi, \eta) \right]^2 \quad (47)$$

3. It is suggested to use  $|| \nabla^4 s(\xi, \eta) ||^2$  as a smoothness measure for a surface. The physical interpretation of the quantity  $\nabla^4 s(\xi, \eta)$  is found in a plate bending theory; an unloaded plate can bend only in a biharmonic function  $\omega$  where

$$\nabla^4 \omega = 0 \quad (48)$$

### Smoothing Integral

Now we need to determine the function  $s(\xi, \eta)$  which minimizes the objective function  $J$  in Eq. (28). It is noted that the smoothing integral in its present form gives difficulties in finding an explicit solution. By evaluating the integrals of the derivatives of basis functions and applying some algebraic manipulations, these smoothing integrals are converted to quadratic forms as follows:

$$\begin{aligned} J_s &= \rho \int_{\eta_1}^{\eta_M} \int_{\epsilon_1}^{\epsilon_N} [z(\xi, \eta)] d\xi d\eta = \rho \sum_{j=1}^{M-1} \sum_{i=1}^{N-1} \int_{\eta_j}^{\eta_{j+1}} \int_{\xi_i}^{\xi_{i+1}} [z(\xi, \eta)] d\xi d\eta \\ &= \sum_{j=1}^{M-1} \sum_{i=1}^{N-1} (x_{i,j}^T, x_{i+1,j}^T, x_{i,j+1}^T, x_{i+1,j+1}^T) \cdot \\ &\quad C \cdot (x_{i,j}^T, x_{i+1,j}^T, x_{i,j+1}^T, x_{i+1,j+1}^T)^T \end{aligned} \quad (49)$$

where  $C$  is a 16 by 16 matrix.

Now we can put the objective function together from Eqs. (28), (45), and (49) as

$$\begin{aligned}
 J &= E[J_C] + J_S \\
 &= \sum_{j=1}^M \sum_{i=1}^N \{ [Hx_{i,j} - m_{ij}]^T \bar{R}_{ij}^{-1} [Hx_{i,j} - m_{ij}] \\
 &\quad + [\tilde{H}_i x_{i,j}]^T \tilde{R}_{ij}^{-1} [\tilde{H}_i x_{i,j}] + [\hat{H}_j x_{i,j}]^T \hat{R}_{ij}^{-1} [\hat{H}_j x_{i,j}] \} \\
 &\quad + \sum_{j=1}^{M-1} \sum_{i=1}^{N-1} [x_{i,j}^T, x_{i+1,j}^T, x_{i,j+1}^T, x_{i+1,j+1}^T]^T \\
 &\quad \cdot C[x_{i,j}^T, x_{i+1,j}^T, x_{i,j+1}^T, x_{i+1,j+1}^T]^T
 \end{aligned} \tag{50}$$

For the optimal values of  $J$ , one can take the partial derivative of  $J$  with respect to the state variables  $x_{i,j}$ , etc. and set to zero.

## CONCLUSIONS

The effect of random angular errors to the range measurement has been studied with the approximating function at the random node modeled. The functional is expressed first in terms of the smooth functions and then in terms of state variables. An expected value of this functional is formulated so that it is in terms of the covariance of the random angular errors. The work has been extended to two-dimensional random grids using bicubic Hermite polynomials.

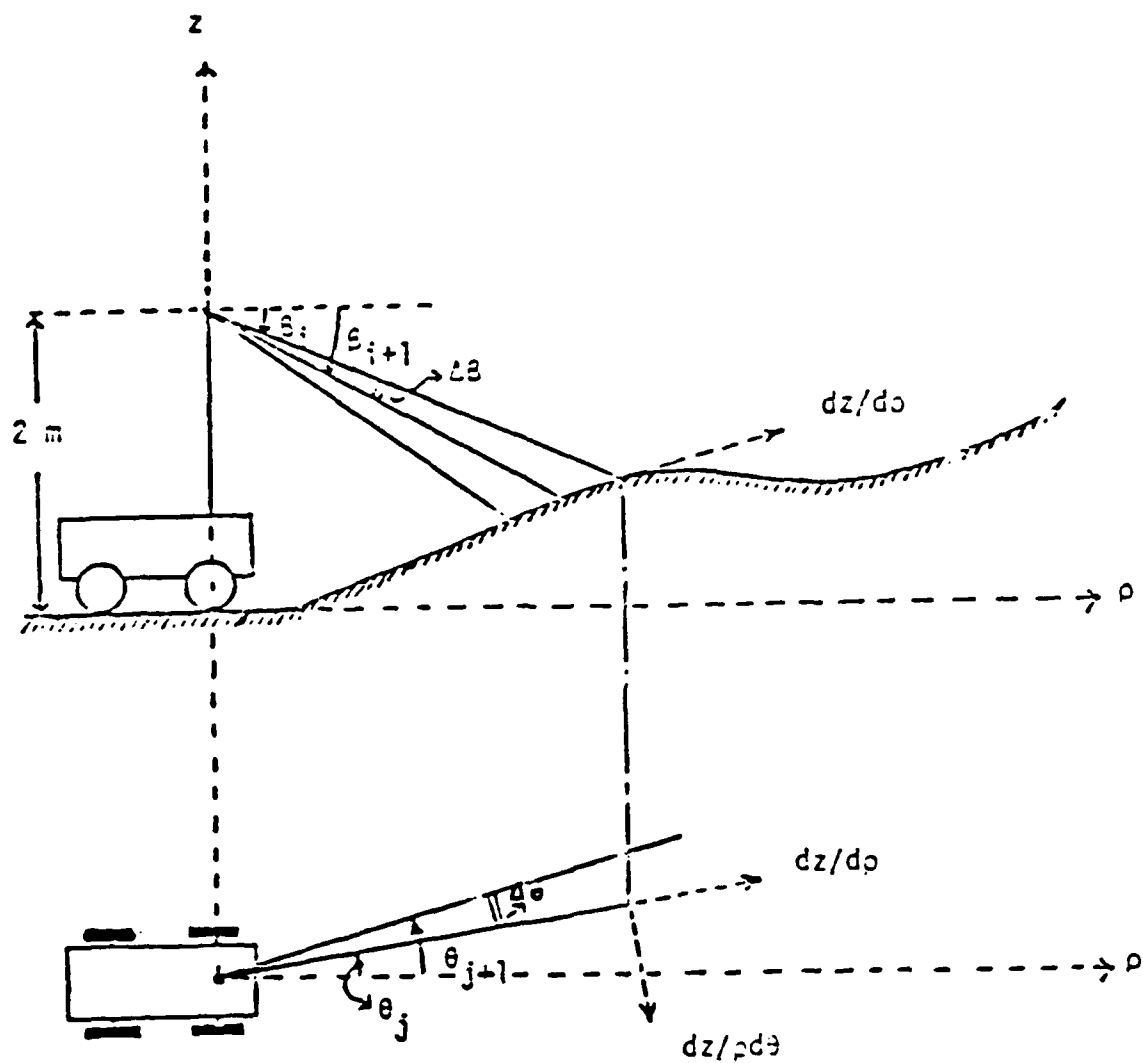


Figure 1. Top and side view of range finder.

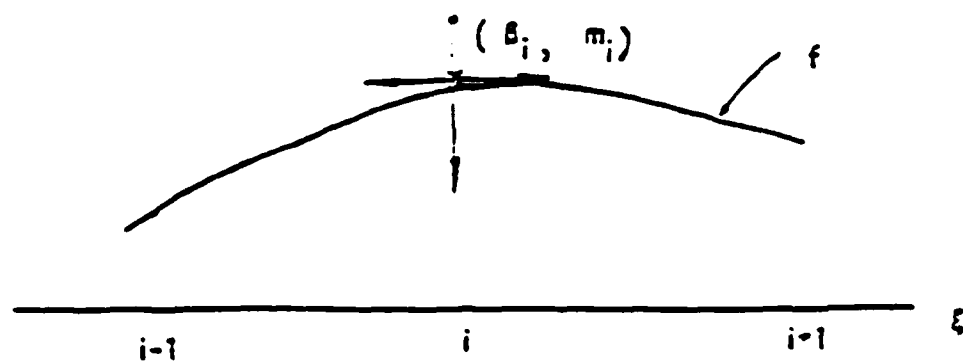


Figure 2. Random noise in angle and range measurements.

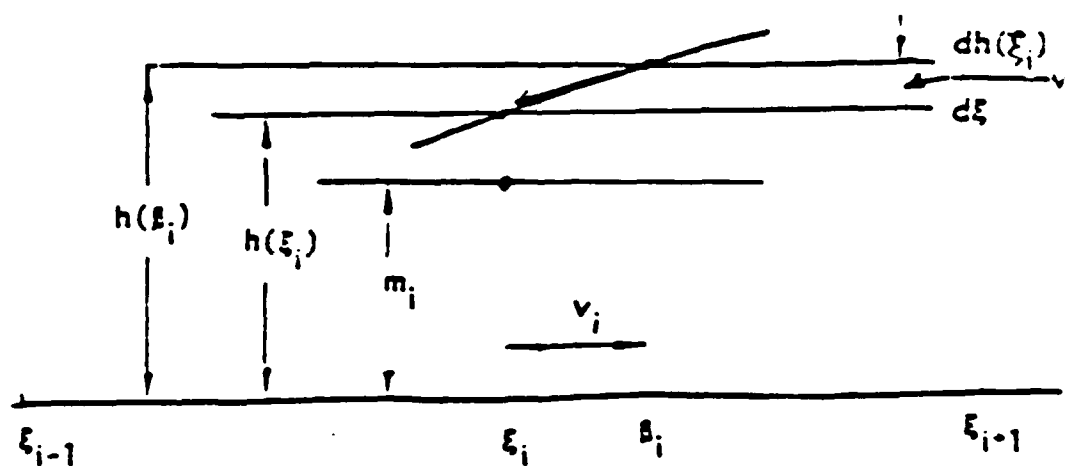


Figure 3. Representation of function due to angular errors.

# TECHNICAL REPORT INTERNAL DISTRIBUTION LIST

	<u>NO. OF COPIES</u>
CHIEF, DEVELOPMENT ENGINEERING BRANCH	
ATTN: SMCAR-CCB-D	1
-DA	1
-DC	1
-DM	1
-DP	1
-DR	1
-DS (SYSTEMS)	1
CHIEF, ENGINEERING SUPPORT BRANCH	
ATTN: SMCAR-CCB-S	1
-SE	1
CHIEF, RESEARCH BRANCH	
ATTN: SMCAR-CCB-R	2
-R (ELLEN FOGARTY)	1
-RA	1
-RM	1
-RP	1
-RT	1
TECHNICAL LIBRARY	5
ATTN: SMCAR-CCB-TL	
TECHNICAL PUBLICATIONS & EDITING UNIT	2
ATTN: SMCAR-CCB-TL	
DIRECTOR, OPERATIONS DIRECTORATE	1
ATTN: SMCWV-OD	
DIRECTOR, PROCUREMENT DIRECTORATE	1
ATTN: SMCWV-PP	
DIRECTOR, PRODUCT ASSURANCE DIRECTORATE	1
ATTN: SMCWV-QA	

NOTE: PLEASE NOTIFY DIRECTOR, BENET WEAPONS LABORATORY, ATTN: SMCAR-CCB-TL, OF ANY ADDRESS CHANGES.

# TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST

	NO. OF COPIES		NO. OF COPIES
ASST SEC OF THE ARMY RESEARCH AND DEVELOPMENT ATTN: DEPT FOR SCI AND TECH THE PENTAGON WASHINGTON, D.C. 20310-0103	1	COMMANDER ROCK ISLAND ARSENAL ATTN: SMCRI-ENM ROCK ISLAND, IL 61299-5000	1
ADMINISTRATOR DEFENSE TECHNICAL INFO CENTER ATTN: DTIC-FDAC CAMERON STATION ALEXANDRIA, VA 22304-6145	12	DIRECTOR US ARMY INDUSTRIAL BASE ENGR ACTV ATTN: AMXIB-P ROCK ISLAND, IL 61299-7260	1
COMMANDER US ARMY ARDEC ATTN: SMCAR-AEE	1	COMMANDER US ARMY TANK-AUTMV R&D COMMAND ATTN: AMSTA-DDL (TECH LIB) WARREN, MI 48397-5000	1
SMCAR-AES, BLDG. 321	1	COMMANDER	
SMCAR-AET-O, BLDG. 351N	1	US MILITARY ACADEMY	1
SMCAR-CC	1	ATTN: DEPARTMENT OF MECHANICS	
SMCAR-CCP-A	1	WEST POINT, NY 10996-1792	
SMCAR-FSA	1		
SMCAR-FSM-E	1	US ARMY MISSILE COMMAND	
SMCAR-FSS-D, BLDG. 94	1	REDSTONE SCIENTIFIC INFO CTR	2
SMCAR-MSI (STINFO)	2	ATTN: DOCUMENTS SECT, BLDG. 4484	
PICATINNY ARSENAL, NJ 07806-5000		REDSTONE ARSENAL, AL 35898-5241	
DIRECTOR US ARMY BALLISTIC RESEARCH LABORATORY ATTN: SLCBR-DD-T, BLDG. 305	1	COMMANDER US ARMY FGN SCIENCE AND TECH CTR ATTN: DRXST-SD	1
ABERDEEN PROVING GROUND, MD 21005-5066		220 7TH STREET, N.E. CHARLOTTESVILLE, VA 22901	
DIRECTOR US ARMY MATERIEL SYSTEMS ANALYSIS ACTV ATTN: AMXSY-MP	1	COMMANDER US ARMY LABCOM	
ABERDEEN PROVING GROUND, MD 21005-5071		MATERIALS TECHNOLOGY LAB ATTN: SLCMT-IML (TECH LIB)	2
COMMANDER HQ, AMCCOM ATTN: AMSMC-IMP-L	1	WATERTOWN, MA 02172-0001	
ROCK ISLAND, IL 61299-6000			

**NOTE:** PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH, DEVELOPMENT, AND ENGINEERING CENTER, US ARMY AMCCOM, ATTN: BENET WEAPONS LABORATORY, SMCAR-CCB-TL, WATERVLIET, NY 12189-4050, OF ANY ADDRESS CHANGES.

# TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST (CONT'D)

	<u>NO. OF COPIES</u>		<u>NO. OF COPIES</u>
<p>COMMANDER US ARMY LABCOM, ISA ATTN: SLCIS-IM-TL 2800 POWDER MILL ROAD ADELPHI, MD 20783-1145</p>	1	<p>COMMANDER AIR FORCE ARMAMENT LABORATORY ATTN: AFATL/MN EGLIN AFB, FL 32543-5434</p>	1
<p>COMMANDER US ARMY RESEARCH OFFICE ATTN: CHIEF, IPO P.O. BOX 12211 RESEARCH TRIANGLE PARK, NC 27709-2211</p>	1	<p>COMMANDER AIR FORCE ARMAMENT LABORATORY ATTN: AFATL/MNG EGLIN AFB, FL 32542-5000</p>	1
<p>DIRECTOR US NAVAL RESEARCH LAB ATTN: MATERIALS SCI &amp; TECH DIVISION CODE 26-27 (DOC LIB) WASHINGTON, D.C. 20375</p>	1 1	<p>METALS AND CERAMICS INFO CTR BATTELLE COLUMBUS DIVISION 505 KING AVENUE COLUMBUS, OH 43201-2693</p>	1

NOTE: PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH, DEVELOPMENT, AND ENGINEERING CENTER, US ARMY AMCCOM, ATTN: BENET WEAPONS LABORATORY, SMCAR-CCB-TL, WATERVLIET, NY 12189-4050, OF ANY ADDRESS CHANGES.

END

10-87

DTIC